

(a) Complete workspace view generated with Monte Carlo method

(b) Vertical section in *yz*-plane with comparison between optimized ray-based and Monte Carlo workspaces

Figure 5.16: Workspace points generated with Monte Carlo method describing NB-R2 workspace and comparison with optimized ray-based process results. Red-yellow points are generated with the Monte Carlo method. Blue-green points are generated with the optimized ray-based method.

(a) Complete workspace view generated with Monte Carlo method

(b) Vertical section in *yz*-plane with comparison between optimized ray-based and Monte Carlo workspaces

Figure 5.17: Workspace points generated with Monte Carlo method describing NB-R3 workspace and comparison with optimized ray-based process results. Red-yellow points are generated with the Monte Carlo method. Blue-green points are generated with the optimized ray-based method.

5.5 Proposed workspace surface plot

After computing the points on the workspace boundaries, it is necessary to interpolate them to generate the workspace surface. This section describes the algorithm to interpolate all the points and plot the workspace surface. This procedure makes it possible later to compute other workspace features like its surface area or volume. Moreover, an automatic process to determine the reachability of a 3D point could be implemented. However, the interpolation process presented here applies only to symmetrical workspaces. This means that only the workspace surfaces of the NB-R1 and NB-R2 can be computed. The NB-R3 workspace has a too complex non-symmetrical shape and can not be interpolated in a surface at the moment. Firstly, the point interpolation and surface generation method is explained. Then, the NB-R1 and NB-R2 workspace surfaces are shown.

This surface plot process is developed using the program MATLAB. Starting from the workspace point cloud, a cubic grid that contains all the points is created in the 3D space using the function meshgrid. This grid comprises several equidistant nodes spread along all the axes *x*, *y* and *z* that will be used for the first part of the process. A smaller step between each node leads to more nodes and a denser grid. Then, the generated points are substituted with the closest node on the previously defined 3D grid. More than one point can be substituted with the same node on the grid. This means there will be at most as many nodes on the workspace boundary as the generated points. So, a denser grid will lead to a more accurate surface plot. Figure [5.18](#page-2-0) shows the selected nodes closer to the determined workspace boundary points. The set of these nodes is called *A* and the coordinates are named (x_A, y_A, z_A) .

Figure 5.18: NB-R1 workspace boundary points in red and selected nodes on grid in blue

The interpolation process starts sectioning the grid along axis *z*. As shown in Fig. [5.19,](#page-3-0) a *xy* section of Fig. [5.18](#page-2-0) shows one or two circumferences for the symmet-

 $z_A = 1.13 \text{ m}$

Figure 5.19: NB-R1 selected nodes on grid for some horizontal sections in *xy*-plane for grid value *z^A* along *z*

Figure 5.20: Reconstructed circumferences with center (x_c, y_c) and radius R_1 and R_2 starting from the NB-R1 selected nodes on grid for some horizontal sections in *xy*plane for grid value *z^A* along *z*

rical workspaces based on the height along *z*. These nodes are identified by $A(z_A)$ where z_A is a grid value along z . They are interpolated to identify the coefficients of two circumferences that pass through the nodes. Only one circumference is considered when the identified circumferences are too close because the nodes form just one circle, as shown in Fig. [5.19b.](#page-3-0) A minimization problem is solved to obtain the coefficients of the circumferences.

$$
\min_{\substack{x_c, y_c, \ x_c, y_c}} \text{avg}\{((x_A - x_c)^2 + (y_A - y_c)^2 - R_1)((x_A - x_c)^2 + (y_A - y_c)^2 - R_2)\}\
$$
\n
$$
\forall (x_A, y_A) \in A(z_A)
$$
\n(5.3)

The Eq. [5.3](#page-4-0) minimize the average distance of each point from the two circumferences identified by the same center (x_c, y_c) and radius R_1 and R_2 . If the difference between R_1 and R_2 is under a certain threshold, only one circumference is considered. This process is repeated $\forall z_A \in A$. The reconstructed circumferences starting from the selected nodes are plotted in Fig. [5.20.](#page-3-1)

At this point, one or two circumferences have been identified on each grid height. The second part of the interpolation process starts and the previous 3D grid is deleted. A new grid is initialized equal to the previous one. All the nodes that compose this new grid are collected in a set called *B* with coordinates named (x_B, y_B, z_B) .

(a) Selected grid nodes at height $z_C = 0.11$ m (b) Selected grid nodes at height $z_C = 1.13 \text{ m}$

Figure 5.21: New selected nodes on grid in coincidence with the obtained circumferences for the NB-R1 workspace for some horizontal sections in *xy*-plane for grid value *z^C* along *z*

Algorithm 5.2 Grid node coefficient assignment

Require: Grid around the desired generated workspace, called *B*, and nodes on grid with coordinates named (x_B, y_B, z_B) . Selected nodes on the workspace boundary *C* with coordinates named (x_C, y_C, z_C) .

- 1: Initialize variable sign $s = -1$.
- 2: **for** $\forall z_B \in B$ **do**

Figure 5.22: Processes of coefficient value assignment to each node in the grid built on the NB-R1 workspace for some horizontal sections in *xy*-plane for grid value *z^B* along *z*. Full procedure explained in Algorithm [5.2.](#page-5-0)

The nodes that coincide with the computed circumferences are also collected in another set called *C* with coordinates (x_C, y_C, z_C) . So, the set *C* is composed of the nodes on the workspace boundaries. Figure. [5.21](#page-4-1) shows the selected nodes that coincide with the circumferences. After this step, a positive or negative coefficient is assigned to each node of the set *B*. This coefficient is equal to the minimum distance *d* between y_B and closest y_C for each couple (x_B, z_B) . A positive coefficient is assigned when the node is inside the workspace and becomes negative for the nodes outside. When y_B and y_C are equal, a 0 value is assigned since that node is on the workspace boundary. Algorithm [5.2](#page-5-0) and Fig. [5.22](#page-5-1) summarizes this procedure.

(b) Internal workspace view

Figure 5.23: Surface of the NB-R1 workspace generated interpolating the points obtained with the workspace determination algorithm

Figure 5.24: Surface of the NB-R2 workspace generated interpolating the points obtained with the workspace determination algorithm

Once, a coefficient is assigned to each node, it is possible to use the isosurface function for generating and plotting the workspace boundary surface. Figure [5.23](#page-6-0) shows the surface of the NB-R1 workspace, both 3D and inner views. In the NB-R1 case, the grid had a step of 0*.*03 m. Figure [5.24](#page-7-0) shows the surface of the NB-R2 workspace, both 3D and inner views. In the NB-R2 case, the grid had a step of 0*.*01 m. The surface has been fully reconstructed and is easy understandable. This method can be applied only to the NB-R1 and NB-R2 robots because they are symmetrical and the circumferences can be used to interpolate the point. The

NB-R3 workspace boundaries have too complex shapes for this interpolation process.

5.6 Discussion about the proposed workspace determination algorithm

This section highlights some limitations of the proposed workspace determination algorithm. The first major limitation is the missing prior knowledge about the analyzed manipulator workspaces. So, there is no way to ensure the correctness of the result obtained by this algorithm. However, one way to check the result correctness is by plotting some robot configuration for each workspace. Figure [5.25](#page-8-0) shows the NB-R1 robot CAD model plotted using ROS RViz tool in two different configurations with the end-effector on the detected boundaries. The obtained workspace points are shown in magenta. Trying to move the robot further, reaching a position outside this workspace is impossible. So, the correctness of the workspace detection is demonstrated by testing. Figures [5.26](#page-9-0) and [5.27](#page-9-1) show the NB-R2 and NB-R3 robot CAD models, respectively, in two different configurations with the end-effector on the detected boundaries. The obtained workspace points are shown in magenta. ROS RViz tool is again employed to plot the robots and their workspaces. The same test can be performed to prove the result fidelity.

The proposed algorithm correctly identified the inner boundaries of the previous

(a) Robot on external boundaries (b) Robot on internal boundaries

Figure 5.25: NB-R1 robot configuration on two collected points by the workspace determination algorithm. Obtained workspace points highlighted in magenta.

(a) Robot on external boundaries (b) Robot on internal boundaries

Figure 5.26: NB-R2 robot configuration on two collected points by the workspace determination algorithm. Obtained workspace points highlighted in magenta.

(a) Robot on external boundaries (b) Robot on internal boundaries

Figure 5.27: NB-R3 robot configuration on two collected points by the workspace determination algorithm. Obtained workspace points highlighted in magenta.

robot workspaces. However, the inner boundary detection can lead to errors when the number of NB-modules increases. Figures [5.28](#page-10-0) and [5.29](#page-10-1) show two Nimbl'Bot robot composed of 12 and 14 NB-modules, respectively. No link or offset is inserted between the NB-modules. These robots can touch their base. Figure [5.30](#page-11-0) shows the vertical sections in *yz*-plane of the generated workspace points for the 12 NB-module robots. The workspace of the 12 NB-module robot has some internal boundaries that are bounded between $y \approx [-0.2, 0.2]$ m and $z \approx [0, 0.5]$ m, shown in Fig. [5.30.](#page-11-0) However, some other points are collected above and below the internal boundaries inside the workspace. These points are not part of the workspace boundaries. However, the robot NB-modules reached their limits when moving towards

Figure 5.28: Nimbl'Bot robot composed of 12 NB-modules

Figure 5.29: Nimbl'Bot robot composed of 14 NB-modules

these points. So, the robot was in a configuration that could not be escaped and the end-effector positions were collected as part of the boundaries. A clearer view of this behavior is shown in Fig. [5.31](#page-11-1) for the 14 NB-module robot. It has no inner boundaries. However, several points were collected by the algorithm.

Figure [5.32](#page-12-0) shows the 12 NB-module robot configuration to reach one of the points collected inside the workspace that are not part of the actual boundaries. The first modules of the robot reach the maximum allowed tilt and the robot can no longer move along the desired direction or escape from the singular configuration. However, the robot could reach the same end-effector linear position with another configuration and move toward it. The same behavior can be noticed for the 14 NB-module robot, as shown in Fig. [5.33.](#page-12-1) Similarly, the robot is stuck on an internal position that does not belong to the workspace boundaries. The limitation explained

Figure 5.30: Vertical section in *yz*-plane of points describing workspace of 12 NBmodule robot

Figure 5.31: Vertical section in *yz*-plane of points describing workspace of 14 NBmodule robot

in this section can generate problems in the correct identification of the manipulator workspaces. Further studies on this limitation should be done to improve the workspace determination process.

Figure 5.32: Configuration of 12 NB-module robot on point inside the workspace which does not belong to the boundaries

Figure 5.33: Configuration of 14 NB-module robot on point inside the workspace which does not belong to the boundaries

5.7 Workspace determination conclusions

This chapter presented a new algorithm for the workspace determination of robotic manipulators. The workspace determination process was evaluated on three kinematic redundant robots. However, it can also be applied to non-redundant manipulators. This process employs the TPIK algorithm and kinematic optimization tasks, namely dexterity and manipulability, for the workspace determination. It is not affected by computational redundancy, like the Monte Carlo based methods, and identifies only the workspace boundaries. The performed tests emphasized the process ability to detect the complete workspace boundaries in a small amount of time. It always took less than ten minutes to produce one workspace. The process lasted less than one minute for the smaller robot, e.g. NB-R2. Moreover, using the kinematic optimization tasks allowed for maintaining better kinematic configurations while moving and prevented the manipulator from ending in singular configurations inside the workspace. In the NB-R3 robot case, the generated map identifies the workspace inner boundaries with less accuracy. However, the workspace shape is perfectly identifiable from the obtained results. The optimized ray-based method results are compared with the ones obtained through pseudo-inverse Jacobian raybased and Monte Carlo methods. The proposed optimized ray-based workspace determination algorithm presents more accurate results than the pseudo-inverse Jacobian ray-based method. It is also faster, more accurate and requires fewer points than the Monte Carlo one. Then, a method for interpolating the points of the NB-R1 and NB-R2 workspaces was proposed. The method can generate the surface for symmetrical workspaces. However, this process can not plot the surface for the NB-R3 workspace. The surface interpolation will be helpful to develop an algorithm to compute the reachability of a 3D point automatically. In fact, this is a complex task to automatize, although it is visually easy. Moreover, the surface generation will allow the computation of the area and volume of the workspace. Finally, two main limitation of the proposed algorithm are discussed. First, there is no prior knowledge about the analyzed robot workspaces. So, it is not possible to determine the result correctness. However, a process was explained to check the obtained results. The second limitation appears when the number of NB-modules that compose the design grows. Over 12 NB-modules, the workspace inner boundaries presents some errors because the robot remained stuck in some internal configurations. Part of the work presented in this chapter was published in [\[GCSL23b\]](#page-26-0).

CHAPTER₆ **Conclusions**

Kinematic redundant manipulators are increasingly used in manufacturing industry, providing important advantages. In fact, there can be multiple possible solutions for the same task since the robot is kinematically redundant. They can work in cluttered environments with many obstacles or collaborate with humans and other robots. Moreover, redundancy can be used to solve tasks simultaneously, such as optimizing different performance indices while performing the main task. However, it is important to recognize that this kinematic redundancy also introduces complexities. The main one is the identification of an algorithm to solve the inverse kinematic model problem. Moreover, analyzing the robot features, like the workspace, and optimizing its design become more complex tasks in the presence of kinematic redundancy. This chapter gives a synopsis of the manuscript content, summarizing the main topics treated during the research, and proposes the future work for each subject.

6.1 Thesis synopsis

The work done in this thesis involved three main topics that are linked by two common threads. These topics are related to the problems that arise with kinematic redundant robots, especially when applied to machining applications. So, the first common thread is the use of kinematic redundant manipulators in trajectorytracking applications. The literature on these robots is revised in the introduction and their main complexities are highlighted. In the manuscript, the kinematic redundant robot composed of the actuation mechanism developed by Nimbl'Bot is employed as example for the performed tests. This actuation mechanism is described and its geometric and kinematic models are exposed. Then, a deeper analysis of the relationship between the mechanism design parameter and its kinematic performance is proposed. The second common thread is the use of an algorithm for the kinematic redundancy resolution to identify the robot configuration for a specific task while optimizing some performance indices. In this research, a task priority based kinematic redundancy resolution algorithm was employed to kinematically control the Nimbl'Bot manipulator. It is called task priority inverse kinematic (TPIK) and exploits the robot redundancy to solve a list of prioritized tasks simultaneously.

The three main subjects that make up the thesis are briefly described below. First, the TPIK algorithm is used to kinematically control the redundant Nimbl'Bot robot following a set of desired trajectories. Since this kinematic control algorithm takes advantage of the redundancy solving simultaneous tasks, three new tasks are introduced. These tasks are based on the kinetostatic performance of the robot, namely dexterity, manipulability and robot transmission ratio (RTR). These tasks are used for the kinetostatic optimization of the robot configuration. In the conducted tests, the robot tracks different given trajectories with and without the optimization tasks. These tests are repeated several times to avoid the attractions to local maxima. The results show a better kinetostatic behavior when the optimization tasks are active. Moreover, the time difference between using or not the optimization tasks is negligible. A new index ϵ is defined as a linear combination of the kinetostatic indices and used to rate the test performance. The value of ϵ is on average 50% higher when reaching the trajectory starting poses activating the optimization tasks. The mean value of ϵ is on average 22% higher along the trajectories when the optimization tasks are active. In general, the kinetostatic performance directly relates to the trajectory placement and the velocity and force vector orientations. Finally, some studies on the linear kinematic Jacobian matrix singular vectors show that the movement effectiveness along the direction \vec{y} is reduced compared to the other axes.

The second topic proposes a method for the design optimization of kinematic redundant robots. Here, the TPIK algorithm is employed to create this novel approach and optimize the design with respect to the desired applications and the kinetostatic indices dexterity, manipulability and RTR. This process considers the optimized design parameters as controllable virtual joints and updates their values while moving the robot. Initially, a simpler case is used to validate the new approach. Only two design variables and two paths are used and the results are compared with a discretized method. The two methods converged to equivalent results, obtaining the same performance, but the new process proposed here requires six time less the total computational time. In fact, the proposed optimization process can identify the best solution for a specific application without testing all the possible design parameter combinations. Later, the proposed method is applied to a case study with more design parameters and trajectories. Several possible Nimbl'Bot robot designs are identified with high kinetostatic performance in the desired workspace area. The algorithm is tested with and without a task based on the center of mass to compare the ending robot dimension difference. When the center of mass task is not used, the resulting designs have high kinetostatic performance but too large dimensions for a real application. When the center of mass task is employed, the obtained designs are smaller, generating some realizable manipulators, but the kinetostatic performance is lower than in the previous case. In conclusion, this design optimization algorithm gives the guidelines for building a performant redundant robot based on a desired application and some performance metrics. Of course, some rate parameters can be antagonistic or not comparable to each other, like the kinetostatic indices and the center of mass distance. So, the user will have to use the guidelines to choose the most suitable result, doing a trade-off between all the application requirements.

The third topic is related to the kinematic redundant robot workspace determination and analysis. The workspace determination process is developed and evaluated on some kinematic redundant designs and employs a ray-based concept. However, it can also be applied to non-redundant manipulators. This process employs the TPIK algorithm and kinematic optimization tasks, namely dexterity and manipulability, for the workspace determination. The goal is to identify the workspace boundaries in a shorter period of time, avoiding the problems that Monte Carlo based methods have facing with. The tests are performed on three Nimbl'Bot designs and the results give a clear map of the workspaces. Each test takes less than ten minutes to produce one workspace and less than one minute for the smaller robot. In the case of robots with non-symmetrical workspaces, the workspace inner boundary profiles are less accurate than in the cases of symmetrical workspaces. Nevertheless, the resulting workspace shape can still be accurately determined based on the outcomes. The optimized ray-based method is compared two other methods, pseudo-inverse Jacobian ray-based and Monte Carlo. The proposed algorithm presents more accurate results than the pseudo-inverse Jacobian ray-based method. It is also faster, more accurate and requires fewer points than the Monte Carlo one. Then, a new point interpolating method for the symmetrical workspaces is introduced to plot the workspace surfaces. The surface generation is helpful to understand more features of the workspace, like calculating its volume or computing the reachability of a 3D point. Two main limitation of the proposed algorithm are discussed. First, there is no prior knowledge about the analyzed robot workspaces. So, it is not possible to determine the result

correctness. However, a process was explained to check the obtained results. The second limitation appears when the number of NB-modules that compose the design grows. Over 12 NB-modules, the workspace inner boundaries presents some errors because the robot remained stuck in some internal configurations.

All the proposed algorithms were tested on several different Nimbl'Bot robotic designs built through a serial connection of the NB-modules. However, these methods can be applied to any type of kinematic redundant manipulator. All the proposed algorithms give promising results and could be further fine-tuned to improve the resulting quality.

6.2 Future work

The work done in this thesis spreads in different fields and opens other subjects. This section presents the future work and analysis for each topic treated in this research.

- 1. **NB-module Modeling and Analysis:** Starting from Chapter 2, the NBmodule geometric and kinematic models were described and analyzed. However, its dynamic model was not treated in this research. Similarly, the stiffness of the NB-module was not modeled. Future analyses should address these topics, which are relevant to demonstrate the abilities and limits of the robots actuated by NB-modules.
- 2. **Task Priority Kinematic Control:** The robot kinetostatic performance was tested by tracking some trajectories in Chapter 3. However, the proposed study uses only four squared trajectories with constant velocities and forces to test the robot performance. So, it is impossible to identify the best placement and orientation for the workpiece. This concept is the starting point for future analysis. Then, the performance of other existing manipulators should be compared with the Nimbl'Bot design one on the same tasks. This comparison should be made later on to present the Nimbl'Bot design potentials with respect to the counterparts. Moreover, the simulation tests could include some obstacles and self-collision avoidance tasks. These tasks allow the robot to work in more complex environments or with other robots. Finally, all the tests were performed in simulation. The TPIK algorithm should be tested on a real prototype of the Nimbl'Bot robot to demonstrate its abilities in real scenarios.
- 3. **Design Optimization Process:** In Chapter 4, the proposed design optimization process provided guidelines to build kinetostatic optimized Nimbl'Bot designs with respect to the desired machining application. Future work could involve further analysis to identify if more general guidelines exist for building a Nimbl'Bot robot design with high kinetostatic performance. For example, this could be done by giving more importance to one index than others or searching for specific relationships between the design parameters. Other design parameters could be included to study how they affect the kinetostatic performance. Moreover, obstacle and self-collision avoidance could be added to the optimization process to consider a more complex environment.
- 4. **Workspace Determination Algorithm:** Regarding the workspace determination algorithm proposed in Chapter 5, the process needs to be revised to improve the non-symmetrical workspace identification. Future work could also address the workspace determination for a specific end-effector orientation. This is important when planning the workpiece placement inside the robot reachable area. Then, a general process to interpolate the workspace points for any robot should be developed, starting from the one already proposed for symmetrical workspaces. So, it should be possible to plot the workspace surface for any Nimbl'Bot design and automatically compute whether a point is inside the workspace. Finally, some additional steps should be added to the workspace determination process to escape the inner boundary identification problem.

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Journal and Conference Publications

- **Title:** Design and Kinematic Analysis of a Novel 2-DoF Closed-Loop Mechanism for the Actuation of Machining Robots
- **Conference:** ASME/IDETC-CIE 2021
- **Date:** August 17 20, 2021
- **Abstract:** The essential characteristics of machining robots are their stiffness and their accuracy. For machining tasks, serial robots have many advantages, like a larger workspace, but they lack the necessary stiffness to accomplish high machining effort tasks. One way to increase the stiffness of serial manipulators is to make their joints using closed-loop or parallel mechanisms instead of using the classical prismatic and revolute joints. This increases the accuracy of a manipulator without reducing its workspace. This paper introduces an innovative two degrees of freedom closed-loop mechanism and shows how this mechanism can be used to build high stiffness and large workspace serial robots. The design of this mechanism is described through its geometric and kinematic models. Then, the kinematic performance of the mechanism is analyzed, and a serial arrangement of several such mechanisms is proposed to obtain a potential design of a machining robot.
- **Reference:** Angelica Ginnante, François Leborne, Stéphane Caro, Enrico Simetti, and Giuseppe Casalino. Design and kinematic analysis of a novel 2-dof closed-loop mechanism for the actuation of machining robots. In *Proceedings of International Design Engineering Technical Conferences and Computers and Information in Engineering Conference*, volume 85444, Online, Virtual, August 17–19 2021. American Society of Mechanical.
- **Title:** Kinetostatic Optimization for Kinematic Redundancy Planning of Nimbl'Bot Robot
- **Journal:** Journal of Mechanism and Robotics (ASME)
- **Date:** March 27, 2023
- **Abstract:** In manufacturing industry, Computer Numerical Control (CNC) machines are often preferred over Industrial Serial Robots (ISR) for machining tasks. Indeed, CNC machines offer high positioning accuracy, which leads to slight dimensional deviation on the final product. However, these machines have a restricted workspace generating limitations in the machining work. Conversely, ISR are typically characterized by a larger workspace. ISR have already shown satisfactory performance in tasks like polishing, grinding and deburring. This paper proposes a kinematic redundant robot composed of a novel two degrees-of-freedom mechanism with a closed kinematic chain. After describing a task priority inverse kinematic control framework used for joint trajectory planning exploiting the robot kinematic redundancy, the paper analyses the kinetostatic performance of this robot depending on the considered control tasks. Moreover, two kinetostatic tasks are introduced and employed to improve the robot performance. Simulation results show how the robot better performs when the optimization tasks are active.
- **Reference:** Angelica Ginnante, Stéphane Caro, Enrico Simetti, and François Leborne. Kinetostatic optimization for kinematic redundancy planning of nimbl'bot robot. *Journal of Mechanisms and Robotics*, 16(3), 2023.
- **Title:** Task Priority Based Design Optimization of a Kinematic Redundant Robot
- **Journal:** Mechanism and Machine Theory
- **Date:** May 9, 2023
- **Abstract:** This paper presents and defines a new design optimization method for kinematic redundant robot manipulators based on their applications. Kinematic redundant manipulators can reach a pose with an infinite number of postures. So, identifying the best robot design and configuration for a set of desired tasks is a highly complex non-linear problem. This approach employs a task priority control algorithm to perform a task oriented robot design optimization. The design parameters are replaced by controllable prismatic or revolute virtual joints and controlled by the algorithm to accomplish the desired tasks. Therefore, this new method finds an optimal robot design for a set of tasks taking advantage of the robot kinematic redundancy. This method is evaluated on a highly kinematic redundant manipulator, which tracks a set of paths with its end-effector while maintaining good kinetostatic performance.
- **Reference:** Angelica Ginnante, Enrico Simetti, Stéphane Caro, and François Leborne. Task priority based design optimization of a kinematic redundant robot. *Mechanism and Machine Theory*, 187:105374, 2023.
- **Title:** Workspace Determination of Kinematic Redundant Manipulators Using a Ray-Based Method
- **Conference:** ASME/IDETC-CIE 2023
- **Date:** August 20 23, 2023
- **Abstract:** Determining the workspace of a robotic manipulator is extremely significant for knowing its abilities and planning the robot application. There exist several techniques for the robot workspace determination. However, these methods usually are affected by computational redundancy, like in the case of Monte Carlo based methods, or their implementation is difficult. Moreover, the workspace analysis of kinematic redundant manipulators is even more complex. This paper introduces a ray-based workspace determination algorithm, easy to implement and not affected by computational redundancy. The proposed method can be applied to any type of serial robot, but it is tested only on spatial kinematic redundant robots. The results show how the approach can clearly determine the boundary of the robot workspace in a short period of time. Finally the time and quality performance of the ray-based method results are compared to the Monte Carlo one demonstrating the improvement of the proposed method.
- **Reference:** Angelica Ginnante, Stéphane Caro, Enrico Simetti, and François Leborne. Workspace determination of kinematic redundant manipulators using a ray-based method. In *Proceedings of International Design Engineering Technical Conferences and Computers and Information in Engineering Conference*. Conference, Boston, Massachusetts, August 20–23 2023. American Society of Mechanical Engineers.

Titre: Conception, analyse et contrôle cinématique de bras robotiques en série hautement redondants **Mots clés:** redondance cinématique, priorité des tâches, performance cinétostatique, optimisation de la conception, analyse de l'espace de travail

Résumé: L'utilisation de manipulateurs robotiques en trois sujets principaux. Le premier sujet condans l'industrie s'est développée au cours des cerne l'utilisation d'un algorithme de résolution de dernières décennies afin d'améliorer et d'accélérer redondance cinématique prioritaire pour la trajecles processus industriels. Les manipulateurs indus-toire de suivi du robot Nimbl'Bot tout en optimisant triels ont commencé à être étudiés pour les tâches ses performances cinétostatiques. Le deuxième d'usinage car ils peuvent couvrir de plus grands sujet est l'optimisation de la conception d'un robot espaces de travail, ce qui augmente la gamme à redondance cinématique en fonction d'une apd'opérations réalisables et améliore la flexibilité. La plication souhaitée et de ses performances cinétosociété Nimbl'Bot a mis au point un nouveau mé-statiques. Pour le troisième sujet, un nouvel algocanisme, ou module, pour construire des robots rithme de détermination de l'espace de travail est modulaires en série plus rigides et plus flexibles proposé pour les manipulateurs redondants cinépour les applications d'usinage. Ce manipulateur matiques. Plusieurs tests de simulation sont proest un robot redondant cinématique à 21 degrés posés et testés sur quelques conceptions de robots de liberté. Cette thèse analyse en profondeur les Nimbl'Bot pour chaque sujet. caractéristiques du robot Nimbl'Bot et est divisée

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Title: Design, analysis and kinematic control of highly redundant serial robotic arms

Keywords: kinematic redundancy, task priority, kinetostatic performance, design optimization, workspace analysis

Abstract: The use of robotic manipulators in indus- three main topics. The first topic regards using try has grown in the last decades to improve and a task priority kinematic redundancy resolution alspeed up industrial processes. Industrial manipula-gorithm for the Nimbl'Bot robot tracking trajectory tors started to be investigated for machining tasks while optimizing its kinetostatic performances. The since they can cover larger workspaces, increasing second topic is the kinematic redundant robot dethe range of achievable operations and improving sign optimization with respect to a desired appliflexibility. The company Nimbl'Bot developed a new cation and its kinetostatic performance. For the mechanism, or module, to build stiffer flexible se-third topic, a new workspace determination algorial modular robots for machining applications. This rithm is proposed for kinematic redundant manipumanipulator is a kinematic redundant robot with 21 lators. Several simulation tests are proposed and degrees of freedom. This thesis thoroughly analy-tested on some Nimbl'Bot robot designs for each sis the Nimbl'Bot robot features and is divided into subjects.

Willing

Titolo: Progettazione, analisi e controllo cinematico di bracci robotici seriali altamente ridondanti **Parole chiave:** ridondanza cinematica, priorità dei task, prestazioni cinetostatiche, ottimizzazione del design, analisi dello spazio di lavoro

Riassunto: L'uso di manipolatori nell'industria è cresciuto negli ultimi decenni per un algoritmo di risoluzione della ridondanza cinmigliorare e velocizzare i processi industriali. I ematica a priorità di compito per la traiettoria di manipolatori industriali hanno iniziato a essere inseguimento del robot Nimbl'Bot, ottimizzando le studiati per le attività di lavorazione, poiché possono coprire spazi di lavoro più ampi, aumentando mento è l'ottimizzazione del design del robot con la gamma di operazioni realizzabili e migliorando la flessibilità. L'azienda Nimbl'Bot ha sviluppato desiderata e alle sue prestazioni cinetostatiche. un nuovo meccanismo, o modulo, per costruire Per il terzo argomento, viene proposto un nuovo robot modulari seriali più rigidi e flessibili per applicazioni di lavorazione. Questo manipolatore è un robot cinematico ridondante con 21 gradi di libertà. Questa tesi analizza a fondo le caratteristiche perimenti in simulazione con alcuni design di robot del robot Nimbl'Bot ed è suddivisa in tre argomenti Nimbl'Bot.

robotici principali. Il primo argomento riguarda l'utilizzo di sue prestazioni cinetostatiche. Il secondo argoridondanza cinematica rispetto a un'applicazione algoritmo di determinazione dello spazio di lavoro per manipolatori cinematici ridondanti. Per ogni argomento vengono proposti e testati diversi es-